

Express Mail No. EL844343774US

PATENT APPLICATION OF

**EVREN ERYUREK
KADIR KAVAKLIOGLU**

ENTITLED

FLOW DIAGNOSTIC SYSTEM

Docket No. R11.12-0749

CROSS-REFERENCE TO RELATED APPLICATIONS

5 This is a Continuation-In-Part of U.S.
application Serial No. 09/257,896, filed February 25,
1999 which is a Continuation-In-Part of U.S.
application Serial No. 08/623,569, filed March 28,
1996, and this application is also a Continuation-In-
10 Part of U.S. application Serial No. 09/383,828, filed
August 27, 1999.

FIELD OF THE INVENTION

The present invention relates to fluid process
15 control systems. In particular, the present invention
relates to diagnostic systems for fluid flow in
process control systems.

BACKGROUND OF THE INVENTION

Fluid flow meters are used in industrial process control environments to measure fluid flow and provide flow signals for flow indicators and controllers. Inferential flow meters measure fluid flow in a pipe by measuring a pressure drop near a discontinuity within the pipe. The discontinuity (primary element) can be an orifice, a nozzle, a venturi, a pitot tube, a vortex shedding bar, a target or even a simple bend in the pipe. Flow around the discontinuity causes both a pressure drop and increased turbulence. The pressure drop is sensed by a pressure transmitter (secondary element) placed outside the pipe and connected by impulse lines or impulse passageways to the fluid in the pipe. Reliability depends on maintaining a correct

calibration. Erosion or buildup of solids on the primary element can change the calibration. Impulse lines can become plugged over time, which also adversely affects calibration.

5 Disassembly and inspection of the impulse lines is one method used to detect and correct plugging of lines. Another known method for detecting plugging is to periodically add a "check pulse" to the measurement signal from a pressure transmitter. This check pulse
10 causes a control system connected to the transmitter to disturb the flow. If the pressure transmitter fails to accurately sense the flow disturbance, an alarm signal is generated indicating line plugging. Another known method for detecting plugging is sensing of both
15 static and differential pressures. If there is inadequate correlation between oscillations in the static and differential pressures, then an alarm signal is generated indicating line plugging. Still another known method for detecting line plugging is to
20 sense static pressures and pass them through high pass and low pass filters. Noise signals obtained from the filters are compared to a threshold, and if variance in the noise is less than the threshold, then an alarm signal indicates that the line is blocked.

25 These known methods rely on providing static pressure sensors or disassembly of the flow meter, increasing complexity and reducing reliability. These known methods do not provide for diagnosing the condition of the primary element. There is thus a need
30 for a better diagnostic technology providing more predictive, less reactive maintenance for reducing cost or improving reliability.

SUMMARY OF THE INVENTION

A flow diagnostic system is disclosed for coupling to a primary flow sensing element via impulse lines. The flow diagnostic system may include a pressure transmitter that couples to the impulse lines
5 and generates digital pressure data representing pressure.

A control system receives the pressure data and provides the pressure data and real time clock readings associated with pressure data to a diagnostic
10 application stored in the flow diagnostic system.

The diagnostic application includes a first algorithm that calculates a difference between the pressure data and a moving average of the pressure data.

15 The diagnostic application also includes a second algorithm that receives the difference and calculates a trained data set of historical pressure data during a training mode and calculates a current pressure data set during a monitoring mode and then generates
20 diagnostic data as a function of the current pressure data set relative to the historical pressure data, which indicates changes in the condition of flow sensing.

The diagnostic application includes a third
25 algorithm that generates a report indicating the diagnostic data.

The diagnostic application can be provided over a network from an application service provider (ASP) or other source and can run on the control system, the
30 ASP or another remote computer.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a schematic illustration of a flow diagnostic system that diagnoses the condition of impulse lines and/or a primary flow element.

FIG. 2 is a schematic illustration of a first
5 embodiment of a control system that is part of a flow diagnostic system.

FIG. 3 is a schematic illustration of a second embodiment of a control system that is part of a flow diagnostic system.

10 FIG. 4 is a block diagram of a diagnostic application.

FIG. 5 is a block diagram of a diagnostic application that diagnoses the condition of impulse lines.

15 FIG. 6 is a block diagram of a diagnostic application that diagnoses the condition of a primary flow element.

FIG. 7 is a flow chart of a process diagnosing the condition of impulse lines.

20 FIG. 8 is a flow chart of a process diagnosing the condition of a primary element.

FIG. 9 is a flow chart of a process of diagnosing the condition of both impulse lines and a primary element.

25 FIG. 10 is a graph of amplitude versus frequency versus time of a process variable signal.

FIG. 11 is a block diagram of a discrete wavelet transformation.

30 FIG. 12 is a graph showing signals output from a discrete wavelet transformation.

FIG. 13 is a diagram showing a simplified neural network.

FIG. 13 is a diagram showing a simplified neural network.

FIG. 14 is a diagram showing a neural network used to provide a residual lifetime estimate.

FIG. 15 is a graph of residual life versus time.

FIG. 16 illustrates a diagnostic fluid flow meter
5 that has a pitot tube for a primary element.

FIG. 17 illustrates a block diagram of a computer platform communicating with a transmitter via a field network.

10 **DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS**

In the present invention, a flow diagnostic system is provided that can diagnose the condition of either the primary element or impulse lines connected to a pressure transmitter. A diagnostic application is
15 downloadable over a network from an application service provider (ASP), or can be obtained from a computer-readable medium such as a CD-ROM or removable disc. The diagnostic application can run on the control system, a remote computer or the ASP and
20 provide a diagnostic report. The diagnostic application runs on a processor that is high powered relative to the low power embedded processor found in the pressure transmitter. With the use of the high powered processor, sophisticated diagnostics can be
25 performed in real time and provide prompt reports to a plant operator about the condition of primary elements or impulse lines or both. There is no need to use processing time on the processor imbedded in the transmitter for diagnostics, and the transmitter can
30 perform its measurement tasks rapidly.

FIG. 1 is a schematic illustration of a generalized example of a flow diagnostic system 100 that diagnoses the condition of impulse lines 104

and/or a primary flow element 106 placed in a fluid piping system 108. The impulse lines 104 and the primary element 106 are referred to collectively as a "pressure generator."

5 The term "pressure generator" as used in this application means a primary element (e.g., an orifice plate, a pitot tube, a nozzle, a venturi, a shedding bar, a bend in a pipe or other flow discontinuity adapted to cause a pressure drop in flow) together
10 with impulse pipes or impulse passageways that couple the pressure drop from locations near the primary element to a location outside the flow pipe. The spectral and statistical characteristics of this pressure presented by this defined "pressure
15 generator" at a location outside the flow pipe to a connected pressure transmitter 82 can be affected by the condition of the primary element as well as on the condition of the impulse pipes. The connected pressure transmitter can be a self-contained unit, or it can be
20 fitted with remote seals as needed to fit the application. A flange on the pressure transmitter 102 (or its remote seals) couples to a flange adapter on the impulse lines 104 to complete the pressure connections in a conventional manner. The pressure
25 transmitter 102 couples to a primary flow element 106 via impulse lines 104 to sense flow. Primary element 106, as illustrated, is an orifice plate clamped between pipe flanges 105.

Pressure transmitter 102 is coupled to the
30 impulse lines 104 and provides pressure data along line 110 to a control system 112. Pressure transmitter 102 is preferably a differential pressure transmitter. Line 110 is typically a conventional 4-20 mA loop that

Sub
B1
10055103-05004
10055103-05004

provides all of the electrical energization for transmitter 102 and also carries digital pressure data representing the pressure sensed by pressure transmitter 102. Pressure transmitter 102 includes an
5 embedded microprocessor that generates the digital pressure data, however, the computing power of the embedded microprocessor is limited by the power available from the 4-20 mA loop. The digital pressure data is typically transmitted in a standard industry
10 format using a digital protocol such as HART, Foundation Fieldbus, Profibus, CAN or the like.

Control system 112 receives the digital pressure data on line 110 and providing the pressure data and real time clock readings associated with pressure data
15 to a diagnostic application stored in the flow diagnostic system 100.

As explained in more detail below, the diagnostic application can be a application 134 that is stored in and running on a processor in control system 112, an
20 application 130 stored in and running on a processor at an application service provider 126, an application 132 stored in and running on a processor in a remote computer 122 or any combination of these locations. In each of these locations, relatively high power
25 computing is available in comparison to the limited computing power available from the embedded processor in transmitter 102. An arrangement where the diagnostic application is stored on one computer (112, 122 or 126) and running on another one of the
30 computers (112, 122, 126) is also contemplated.

The diagnostic application (134, 130, 132 or a combination of 134, 130 or 132) includes a first algorithm calculating a difference between the

00540-0504
40309-2072900

pressure data and a moving average of the pressure data. The diagnostic application further includes a second algorithm receiving the difference and calculating a trained data set of historical pressure data during a training mode and calculating a current pressure data set during a monitoring mode and generating diagnostic data as a function of the current pressure data set relative to the historical pressure data indicating changes in the condition of flow sensing. The diagnostic application also includes a third algorithm generating a report indicating the diagnostic data. The report can be presented to an user at control system monitor 114, a printer 124 or monitor associated with remote computer 122 or a report 128 generated by the application service provider 126. It is appreciated that the report can take a variety of forms or displays that communicate the diagnostic data to the user.

The control system 112 couples along line 118 to a network 116. Network 116 also couples along line 120 to the remote computer 122, and couples along line 127 to the application service provider 126. Typically, the remote computer 122 is located in the offices of the plant operator, while the line 127 is a long distance connection, typically over the internet, to an application service provider 126 at any desired location.

The network 116 can provide the diagnostic application to the control system 112 or the remote computer 122. The network can also provide the pressure data and associated real time clock readings to the diagnostic application running at the remote computer 122 or the application service provider 126.

The illustration in FIG. 1 is a generalized illustration, and not all diagnostics systems include all of the features shown in FIG. 1.

FIG. 2 is a schematic illustration of a first embodiment of a control system 206 that is part of a flow diagnostic system such as flow diagnostic system 100 in FIG. 1.

Pressure transmitter 200 is coupled via impulse lines 201 to an integral orifice plate 202 in a fluid flow system. Pressure transmitter 200 couples to control system 206 along line 204. The pressure transmitter generates digital pressure data (P) and associated digital real time clock readings (RTC) as illustrated at 205. The real time clock readings provided by the transmitter 200 with each pressure reading indicate the relative time that each pressure reading is taken by the transmitter 200. In an instance where the transmitter generates pressure readings at a generally constant rate, the real time clock reading can be as simple as a sequential number for each reading. In an instance where the pressure reading are somewhat more irregularly spaced in time, the real time clock reading can be an approximate time that each reading taken.

The control system 206 receives the digital information 205 at a transmitter bus interface 208. Transmitter bus interface 208 formats the data properly for communication on the bus 210 that is internal to the control system 206. The information 205 is used by process control software 214 to couple control signals along line 215 to a valve or other control device. Control system 206 includes a network interface 212 that can pass the digital information

205 along to a network on line 218 in a case where the diagnostic application is not running on the control system 206. In a case where the diagnostic application is running on the control system 206, the network interface 212 can receive the diagnostic application from line 218 and format it for transmission over the bus 210. The network interface 212 is bidirectional. The control system 206 includes a processor, random access memory, non-volatile memory and I/O devices.

10 In FIG. 2, the transmitter 200 provides real time clock readings. As explained below in connection with FIG. 3, a flow diagnostic system can also operate with a transmitter that does not provide real time clock readings.

15 FIG. 3 is a schematic illustration of a second embodiment of a control system 306 that is part of a flow diagnostic system such as flow diagnostic system 100 in FIG. 1.

Pressure transmitter 300 is coupled via impulse lines 301 to an integral orifice plate 302 in a fluid flow system. Pressure transmitter 300 couples to control system 306 along line 304. The pressure transmitter generates digital pressure data (P) as illustrated at 305. Transmitter 300 may or may not generate real time clock readings, depending on the design of the transmitter.

In an instance where the transmitter 300 generates real time clock readings, these reading are coupled through transmitter bus interface 308 to real time clock circuit 318 via a bus 310 that is internal to control system 306. Real time clock circuit 318 then generates a corresponding synchronized real time clock reading that is synchronized with other real

time clock readings in the control system 306. This synchronization allows for synchronized comparison of data from multiple transmitters, for example, in a case where differential pressure is measured using two absolute pressure transmitters.

In an instance where transmitter 300 does not generate any usable real time clock readings, then real time clock circuit 318 generates synchronized real time clock readings based on the time that the each pressure data point 305 is received by real time clock circuit 318.

In either instance, the pressure data and synchronized real time clock readings can be used by process control software 314 to couple control signals along line 315 to a valve or other control device. Control system 306 includes a network interface 312 that can pass digital information (pressure data 305 and synchronized real time clock readings) along to a network on line 318 in a case where the diagnostic application is not running on the control system 306. If the network connected to line 318 is busy or otherwise unavailable, then the digital information can be temporarily stored in storage device 320 and later transmitted via the network to a diagnostic application running on a remote computer. This storage 320 can also be used in instances where it is desired to use batch processing for diagnostics.

In a case where the diagnostic application is running on the control system 306, the network interface 312 can receive the diagnostic application from line 318 and format it for transmission over the bus 310 internal to control system 306.

2025-03-04 10:00:00

FIG. 4 is a block diagram of a diagnostic application 432 running on a remote computer 422. Pressure data and real time clock reading from a pressure transmitter are provided on line 320 from a network 316.

A first algorithm 440 stored in computer 422 calculates a difference between the series of digital pressure data points received from network 316 and a moving average of the series of digital pressure data points. Real time clock readings associated with each digital pressure data point are used to ensure that the digital pressure data points, which may be delayed or out of order after passing through network 316, are reassembled in a correct time sequence at the input to algorithm 440. The difference calculated in algorithm 440 is coupled along line 442 to a second algorithm 444.

The second algorithm 444 is also stored in the computer 422. The second algorithm 444 receives the difference calculated by algorithm 440 and calculates a trained data set of historical data during a training mode and calculates a current data set during a monitoring mode and generates diagnostic data 446 as a function of the current data set relative to the historical data indicating changes in the condition of the pressure generator (not illustrated in FIG. 4).

A third algorithm 448 receives the diagnostic data 446 and generates a report 450 indicating the diagnostic data to a user. The report 450, as explained above, can take forms such as a monitor display or a printed report.

FIG. 5 is a block diagram of a diagnostic application running on a remote computer 522 that diagnoses the condition of impulse lines.

In FIG. 5, a difference (subtract moving average) algorithm 540 receives digital pressure data from network 516 via line 520 and generates difference data on line 542 representing a sensed pressure minus a moving average of the sensed pressure. A calculate algorithm 552 receives the difference data from line 542 and calculates a trained output 553 of historical data obtained during a training mode or time interval. After training, calculate algorithm 554 calculates a monitor output 555 of current data obtained during a monitoring mode or normal operation time of the fluid flow meter.

In FIG. 5, a diagnostic algorithm 556 receives the trained output 553 and the monitor output 555 and generates a diagnostic data output 558 indicating a current condition of the pressure generator relative to an historical condition. In FIG. 5, calculate algorithm 554 stores the historical data in memory for later use in the comparison.

In difference algorithm 540, the moving average is calculated according to the series in Eq. 1:

25

$$A_j = \sum_{k=0}^m (P_{j+k}) (W_k) \quad \text{Eq. 1}$$

where A is the moving average, P is a series of sequentially sensed pressure values, and W is a numerical weight for a sensed pressure value, m is a number of previous sensed pressure values in the series. Provision can also be made in difference

circuit 540 to filter out spikes and other anomalies present in the sensed pressure. In FIG. 5, the historical data comprises statistical data, for example, the mean (μ) and standard deviation (σ) of the difference output or other statistical measurements, and the diagnostic output 558 indicates impulse line plugging. The diagnostic application switches between a training mode when it is installed and a monitoring mode when it is in use measuring flow as illustrated by switch 550. The calculate algorithm 554 stores historical data in the training mode. The diagnostic data output 558 indicates a real time condition of the pressure generator.

In FIG. 5, statistical data, such as the mean μ and standard deviation σ , are calculated based on a relatively large number of data points or flow measurements. The corresponding sample statistical data, such as sample mean \bar{X} and sample standard deviation s , are calculated from a relatively smaller number of data points. Typically, hundreds of data points are used to calculate statistical data such as μ and σ , while only about 10 data points are used to calculate sample statistical data such as \bar{X} and s . The number of data points during monitoring is kept smaller in order to provide diagnostics that is real time, or completed in about 1 second. Diagnostic algorithm 556 indicates line plugging if the sample standard deviation s deviates from the standard deviation σ by a preset amount, for example 10%.

FIG. 6 is a block diagram of a diagnostic application running on a remote computer 622 that diagnoses the condition of a primary flow element. The

diagnostic application of FIG. 6 is arranged generally along the lines of the diagnostic application of FIG. 5. A difference algorithm 640 receives digital pressure data from network 616 via line 620. The diagnostic application switches between a training mode and a monitoring mode by switch 650.

In FIG. 6, the diagnostic output 658 indicates a condition of the primary element, while in FIG. 5, the diagnostic output 558 indicates a condition of the impulse lines. In FIG. 6, calculate algorithms 652, 654 calculate and store data on power spectral density (PSD) of the difference output on line 642 rather than statistical data which is used in FIG. 5.

The power spectral density data is preferably in the range of 0 to 100 Hertz. The center frequency of a bandpass filter can be swept across a selected range of frequencies to generate a continuous or quasi-continuous power spectral density as a function of frequency in a manner that is well known. Various known Fourier transforms can be used.

Power spectral density, F_i , can also be calculated using Welch's method of averaged periodograms for a given data set. The method uses a measurement sequence $x(n)$ sampled at f_s samples per second, where $n = 1, 2, \dots, N$. A front end filter with a filter frequency less than $f_s/2$ is used to reduce aliasing in the spectral calculations. The data set is divided into $F_{k,i}$ as shown in Eq. 2:

$$F_{k,i} = (1/M) \left| \sum_{n=1}^M x_k(n) e^{-j2\pi i \Delta f n} \right|^2 \quad \text{Eq. 2}$$

There are $F_{k,i}$ overlapping data segments and for each segment, a periodogram is calculated where M is the number of points in the current segment. After
5 all periodograms for all segments are evaluated, all of them are averaged to calculate the power spectrum:

$$F_i = (1/L) \sum_{k=1}^L F_{k,i} \quad \text{Eq. 3}$$

10

Once a power spectrum is obtained for a training mode, this sequence is stored in memory, preferably EEPROM, as the baseline power spectrum for comparison to real time power spectrums. F_i is thus the power
15 spectrum sequence and i goes from 1 to N which is the total number of points in the original data sequence. N , usually a power of 2, also sets the frequency resolution of the spectrum estimation. Therefore, F_i is also known as the signal strength at the i^{th}
20 frequency. The power spectrum typically includes a large number points at predefined frequency intervals, defining a shape of the spectral power distribution as a function of frequency.

In the detection of the primary element
25 degradation, a relatively larger sample of the spectral density at baseline historical conditions and a relatively smaller sample of the spectral density at monitoring conditions are compared. The relatively smaller sample allows for a real time indication of
30 problems in about 1 second. An increase in the related frequency components of the power spectrum can indicate the degradation of the primary element. Using

The algorithm starts at 702. A moving average is subtracted from differential pressure data as shown at 704 to calculate a difference. During a train mode, historical data on the calculated difference is acquired and stored at 706 as statistical data μ and σ , for example. During an operational MONITOR mode, current data on the difference is acquired and stored at 708 as statistical data \bar{X} and s . The smaller sample of current data is compared to the larger sample of the historical data to diagnose the condition of the impulse lines. Comparisons 710 of historical and current statistical data are made at 714, 716, 718 and a selected diagnostic output is generated at 730, 732, 734 as a function of the comparisons made at 712, 714, 716, 718 respectively.

After completion of any diagnostic output, the process loops back at 720, 722, 724, 726 or 728 to repeat the monitor mode diagnostics, or the

transmitter can be shut down until maintenance is performed. If the diagnostic process itself fails, an error indication is provided on the diagnostic output at 736. In the method of diagnosis illustrated in FIG. 7, the historical data set comprises statistical data such as data on the mean (μ) and standard deviation (σ) of the calculated difference; the current data set comprises current sample statistical data, such as the sample average (\bar{X}) and sample deviation (s) of the calculated difference. The sample deviation (s) is compared to the standard deviation (σ) to diagnose impulse line plugging, for example. Other known statistical measures of uncertainty, or statistical measures developed experimentally to fit this application can also be used besides mean and standard deviation. When there is an unusual flow condition where \bar{X} is much different than μ , the diagnostics can be temporarily suspended as shown at 712 until usual flow conditions are reestablished. This helps to prevent false alarm indications.

In FIGS. 1-7, the transmitter generates a calibrated output and the flow diagnostic system generates a diagnostic output that indicates if the pressure generator is out of calibration. In FIGS. 1-7, the primary element can comprise, for example, a simple pitot tube or an averaging pitot tube as illustrated below in the example shown in FIG. 16. The primary element and impulse pipes can be combined in an integral orifice such as illustrated in FIGS 2-3. An orifice plate adapted for clamping between pipe flanges is illustrated in FIG. 1. The primary element can comprise a venturi, a nozzle or an orifice (not illustrated). A standard arrangement of a pressure

generator can be used with a flow diagnostic system that is adapted to provide the diagnostics outputs. The flow diagnostic system adapts itself to the characteristics of the pressure generator during the training mode and has a standard of comparison stored during the training mode that is available for comparison during the monitoring or operational mode. The standard of comparison can be adjusted as needed by a technician via the network. In each arrangement, the fluid flow meter provides a calibrated flow rate output and the diagnostic report indicates if the pressure generator is out of calibration.

FIG. 8 is a flow chart of a process diagnosing the condition of a primary element.

The condition of the primary element can include erosion or fouling of the primary element. The method or algorithm starts at 802. Digital pressure data is gathered in a training mode or time interval as shown at 804. A power spectrum of the sensor data, minus the moving average, is calculated at 806. The power spectrum obtained is identified as the training power spectrum at 808 and stored in non-volatile memory 810. After completion of training, the process moves on to monitoring or normal use. A further power spectrum of current pressure data, minus the moving average, is evaluated at 812, and the power spectrum so obtained is stored in memory 814, that can be either RAM or nonvolatile memory. At 816, the power spectrum F_i obtained during training is compared to the power spectrum $\underline{F_i}$ obtained during monitoring. If there is a significant difference between F_i and $\underline{F_i}$ which is indicative of a problem with the primary element, a primary element warning (PE Warning) is generated as

5
10

15
20
25

30

large enough to indicate a problem with the primary element, then a PE Warning is generated as shown at 916. If the differences in the power spectral densities are small, then no PE warning is generated
5 as shown at 918. Program flow continues on at 920 to repeat the IL and PE diagnostics, or the flow meter can be shut down if there is a PE or IL warning until maintenance is performed.

Any of the methods can be stored on a computer-
10 readable medium as a plurality of sequences of instructions, the plurality of sequences of instructions including sequences that, when executed by a diagnostic application in a flow diagnostic system, cause the flow diagnostic system to perform a
15 diagnostic method relative to a primary element and impulse lines coupled to the transmitter.

The flow diagnostics system can also be used with a transmitter (not illustrated) which includes remote seals connected by flexible capillary tubes that are
20 filled with a controlled quantity of isolation fluid such as silicone oil. The isolator arrangement permits the transmitter electronics to be spaced away from extremely hot process fluids which contact the remote seals. The flow diagnostics system can also be used to
25 detect leaking and pinching off of capillary tubes using the diagnostic techniques described above to provide diagnostic data.

The flow diagnostics system can also be used with a transmitter (not illustrated) which connects to taps
30 near the bottom and top of a tank. The transmitter provides an output that represents a time integral of flow in and out of the tank. The transmitter includes circuitry, or alternatively software, that measures

00540 0004

the differential pressure between the taps and computes the integrated flow as a function of the sensed differential pressure and a formula stored in the transmitter relating the sensed pressure to the quantity of fluid in the tank. This formula is typically called a strapping function and the quantity of fluid which has flowed into or out of the tank can be integrated as either volumetric or mass flow, depending on the strapping function stored in transmitter. The transmitter can be located either near the bottom or the top of tank, with a tube going to the other end of the tank, often called a "leg." This leg can be either a wet leg filled with the fluid in the tank, or a dry leg filled with gas. Remote seals can also be used with such a transmitter.

In one embodiment, the flow diagnostic system includes a signal preprocessor algorithm that isolates signal components in the pressure data such as frequencies, amplitudes or signal characteristics which are related to a plugged impulse line or degraded primary element. The signal preprocessor provides an output to a signal evaluator in the difference algorithm. The signal preprocessor isolates a portion of the signal by filtering, performing a wavelet transform, performing a Fourier transform, use of a neural network, statistical analysis, or other signal evaluation techniques. Such preprocessing is preferably implemented in the difference algorithm or in a specialized digital signal processor.

The signal components are isolated through signal processing techniques in which only desired frequencies or other signal characteristics such as amplitude are identified and an indication of their

identification is provided. Depending upon the strength signals to be detected and their frequency, signal preprocessor can comprise a filter, for example a band pass filter, to generate the isolated signal output. For more sensitive isolation, advanced signal processing techniques are utilized such as a Fast Fourier transform (FFT) to obtain the spectrum of the sensor signal. In one preferred embodiment, the signal preprocessor comprises a wavelet processor which performs a wavelet analysis on the sensor signal as shown in FIGS. 10, 11 and 12 using a discrete wavelet transform. Wavelet analysis is well suited for analyzing signals which have transients or other non-stationary characteristics in the time domain. In contrast to Fourier transforms, wavelet analysis retains information in the time domain, i.e., when the event occurred.

Wavelet analysis is a technique for transforming a time domain signal into the frequency domain which, like a Fourier transformation, allows the frequency components to be identified. However, unlike a Fourier transformation, in a wavelet transformation the output includes information related to time. This may be expressed in the form of a three dimensional graph with time shown on one axis, frequency on a second axis and signal amplitude on a third axis. A discussion of wavelet analysis is given in On-Line Tool Condition Monitoring System With Wavelet Fuzzy Neural Network, by L. Xiaoli et al., 8 JOURNAL OF INTELLIGENT MANUFACTURING pgs. 271-276 (1997). In performing a continuous wavelet transformation, a portion of the sensor signal is windowed and convolved with a wavelet function. This convolution is performed

202501020000

by superimposing the wavelet function at the beginning of a sample, multiplying the wavelet function with the signal and then integrating the result over the sample period. The result of the integration is scaled and provides the first value for continuous wavelet transform at time equals zero. This point may be then mapped onto a three dimensional plane. The wavelet function is then shifted right (forward in time) and the multiplication and integration steps are repeated to obtain another set of data points which are mapped onto the 3-D space. This process is repeated and the wavelet is moved (convolved) through the entire signal. The wavelet function is then scaled, which changes the frequency resolution of the transformation, and the above steps are repeated.

FIG. 10 is a graph of amplitude versus frequency versus time of a process variable signal such as the pressure data reading from a pressure transmitter. Data from a wavelet transformation of digital pressure data is shown in FIG. 10. The data is graphed in three dimensions and forms a surface 170. As shown in the graph of FIG. 10, the digital pressure data includes a small signal peak 172 at about 1 kHz at time t_1 and another peak 174 at about 100 Hz at time t_2 . Through subsequent processing by the signal evaluator, surface 170 or portions of surface 170 are evaluated to determine impulse piping or primary element degradation.

The continuous wavelet transformation described above requires extensive computations. Therefore, in one embodiment, a discrete wavelet transform (DWT) which is well suited for real time implementation in a control system or personal computer is performed. One

62

[illegible]

Sub B2 enc 1
5 approximately the same as the sensor or the same as the minimum signal resolution required to monitor the signal. Each level of DWT coefficients is representative of signal amplitude as a function of time for a given frequency range. Coefficients for each frequency range are concatenated to form a graph such as that shown in FIG. 10.

10 In some embodiments, padding is added to the signal by adding data to the sensor signal near the borders of windows used in the wavelet analysis. This padding reduces distortions in the frequency domain output. This technique can be used with a continuous wavelet transform or a discrete wavelet transform. "Padding" is defined as appending extra data on either
15 side of the current active data window, for example, extra data points are added which extend 25% of the current window beyond either window edge. In one embodiment, the padding is generated by repeating a portion of the data in the current window so that the
20 added data "pads" the existing signal on either side. The entire data set is then fit to a quadratic equation which is used to extrapolate the signal 25% beyond the active data window.

FIG. 12 is a graph showing signals output from a
25 discrete wavelet transformation (DWT) such as that shown in FIG. 11. FIG. 12 illustrates an example showing a signal S generated by a pressure transmitter and the resultant approximation signals yielded in seven decomposition levels labeled level 1 through
30 level 7. In this example, signal level 7 is representative of the lowest frequency DWT coefficient which can be generated. Any further decomposition yields noise. All levels, or only those levels which

relate impulse piping or primary element degradation are provided.

The algorithm evaluates the isolated signal received from the signal preprocessing and in one embodiment, monitors an amplitude of a certain frequency or range of frequencies identified and provides a diagnostic output if a threshold is exceeded. Signal evaluator can also comprise more advanced decision making algorithms such as fuzzy logic, neural networks, expert systems, rule based systems, etc. Commonly assigned U.S. Patent Application No. 08/623,569 describes various decision making systems which can be implemented in a signal evaluator and is incorporated herein by reference.

The diagnostic application performs diagnostics related to the impulse piping or primary element using information derived from a differential pressure sensor. The following describes a number of embodiments for realizing a diagnostic application. The diagnostic application can provide a residual lifetime estimate, an indication of a failure, an indication of an impending failure or a calibration output which is used to correct for errors in the sensed process variable.

A. POLYNOMIAL CURVEFIT

In one embodiment of the present invention empirical models or polynomial curve-fitting are used to detect line plugging or primary element degradation. A polynomial-like equation which has a combination of input signals such as various statistical parameters can be used to detect primary element degradation or impulse line plugging.

Constants for the equations can be stored in a memory or received over the network.

B. NEURAL NETWORKS

The signal can be analyzed using a neural
5 network. One such neural network is a multi-layer
neural network. Although a number of training
algorithms can be used to develop a neural network
model for different goals. One embodiment includes the
known Backpropagation Network (BPN) to develop neural
10 network modules which will capture the nonlinear
relationship among a set of input and output(s).

FIG. 13 is a diagram showing a simplified neural
network. FIG. 13 illustrates a typical topology of a
three-layer neural network architecture that can be
15 implemented in the diagnostic application. The first
layer 270, usually referred to as the input buffer,
receives the information, and feeds them into the
inner layers. The second layer, in a three-layer
network, commonly known as a hidden layer 272,
20 receives the information from the input layer,
modified by the weights on the connections 274 and
propagates this information forward. This is
illustrated in the hidden layer 272 which is used to
characterize the nonlinear properties of the system
25 analyzed. The last layer is the output layer 276 where
the calculated outputs (estimations) are presented to
the environment.

FIG. 14 is a diagram showing a neural network 280
used to provide a residual lifetime estimate. FIG. 14
30 illustrates a schematic of a neural network which
provides a residual life estimate 282 for a primary
element or impulse pipe based upon a sensor
(transmitter) signal 284. The sensor signal can be

FOUO 20125800

either a raw sensor signal or a sensor signal which has been processed through signal processing techniques.

FIG. 15 is a graph 290 of residual life 292 versus time 294. FIG. 15 illustrates a graph of residual life versus time and shows that an alarm level 296 can be set prior to an estimated failure time 298. This allows the system to provide an alarm output prior to actual failure of the device.

10 C. THRESHOLD CIRCUITRY

This embodiment uses a set of if-then rules to reach a conclusion on the status of the impulse piping or primary element. This embodiment may be implemented easily in analog or digital circuitry. For example, 15 with a simple rule, if the signal drops a certain amount below a historical mean, an output can be provided which indicates that an impulse line is plugged or is in the process of becoming plugged. Of course, more complex rules can be used which use 20 multiple statistical parameters or signal components of the sensor signal to provide more accurate or different information.

D. WAVELETS

With this embodiment, one or more of the 25 decomposition signal(s) in a wavelet analysis directly relate to line plugging and are used to diagnose the transmitter.

FIG. 16 illustrates a diagnostic fluid flow meter that has a pitot tube for a primary element. The 30 primary element can comprise a simple pitot tube or an averaging pitot tube as illustrated. The pitot tube 190 can be inserted through a tap 192 on a pipe 194. An instrument manifold 196 can couple between the

pressure generator (including pitot inlets and impulse pipes internal to the pitot tube 190) and a pressure transmitter 198.

FIG. 17 illustrates a computer platform 1 that connects via an interface 2 to one of several Hart interchange Devices 4. Interface 2 can be an RS232-RS485 converter, an ethernet connection, an intranet or internet connection, or other suitable interface that communicates information to the computer platform 1. The computer platform 1 is typically a personal computer located in a maintenance shop area that includes application software such as an Asset Management Solutions (AMS) software application from Rosemount Inc. Each Hart interchange devices 4 couples to one or more pressure transmitters 6 via a termination panel 8. The Hart interchange devices 4 are coupled via a DIN rail or bus 10 to a control system 12. A diagnostic application 14 as described above in connection with FIGS. 1-16 also resides on computer platform 1. Computer platform 1 provides a diagnostic report as explained above. The arrangement illustrated in FIG. 17 allows substantially all of the diagnostic software to run on computer platform 1 (which is a small control system) rather than place additional overhead on control system 12. The term "control system" as used in this application includes control systems such as control system 112 in FIG. 1 which provide electrical feedback to a fluid processing plant as well as computers that perform a monitoring function such as computer platform 1, where the feedback to the fluid processing plant comprises human intervention based on a diagnostic report generated by the computer platform 1.

FIG. 17

